



Low-cost Prototype Pyrgeometer for Atmospheric Radiation Measurements

Prototipo de pirgeómetro de bajo costo para mediciones de radiación atmosférica

Yuber Otálora-Porras ¹, Cristian Camilo Serrano-Franco ², César Alexander Chacón-Cardona ³

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Abstract

Objective: To design and build an instrument capable of measuring long-wave infrared radiation with elements of the national market that offers an excellent performance in measuring energy in this spectral band.

Methodology: The best design was determined based on other existing instruments, innovating its development by using materials that are easily accessible in the country, and its operation was verified by characterizing an incandescent light bulb used as an infrared radiation pattern. Then, the radiation measured by the instrument was compared to that emitted by the source by means of an experimental setup that involved measuring the temperature at several distances.

Results: A functional prototype was obtained, and its operation could be verified through a series of irradiance measurements according to the Stefan-Boltzmann law, through a calibration process with a known radiation source.

Conclusions: A radiometric instrument for the thermal infrared band was designed and built. Raw materials and electronic components were used which were available in the local market, thus noticeably reducing the equipment's production costs.

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Keywords: emissivity, black body, thermal radiation, irradiance, pyrgeometer.

¹Student of the Electronics Technician program (propaedeutic cycles). Student, Universidad Distrital Francisco José de Caldas, Bogotá, Colombia.

Email: yuotalorap@correo.udistrital.edu.co

²Student of the Electronics Technician program (propaedeutic cycles). Student, Universidad Distrital Francisco José de Caldas, Bogotá, Colombia.

Email: cserranof@correo.udistrital.edu.co

³Posgraduate studies: Master's and Doctoral Degrees in Science, Physics; Undergraduate studies: physicist. Assistant professor at Universidad Distrital Francisco José de Caldas and member of the Electromagnetic Compatibility (CEM) research group, Bogotá D.C, Colombia.

Email: cachaconc@udistrital.edu.co

Resumen

Objetivo: Diseñar y construir un instrumento capaz de medir la radiación infrarroja de onda larga con elementos del mercado nacional que ofrezca un excelente desempeño en la cuantificación de energía en esta banda espectral.

Metodología: Se determinó el mejor diseño, basado en otros instrumentos ya existentes, innovando su desarrollo mediante el uso de materiales de fácil acceso en el país, y se comprobó su funcionamiento mediante la caracterización de una bombilla incandescente usada como patrón de radiación infrarroja. Luego se comparó la radiación medida por el instrumento con la radiación emitida por la fuente mediante un montaje experimental en el que se midió la temperatura a diversas distancias.

Resultados: Se obtuvo un prototipo funcional, siendo posible constatar su funcionamiento mediante una serie de medidas de irradiancia en consonancia con la ley de Stefan-Boltzmann, a través de un proceso de calibración con una fuente de radiación conocida.

Conclusiones: Se diseñó y construyó un instrumento radiométrico para la banda espectral del infrarrojo térmico. Se emplearon materias primas y componentes electrónicos disponibles en el medio local, reduciendo notablemente los costos de producción del equipo.

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Palabras clave: emisividad, cuerpo negro, radiación térmica, irradiancia, pirgeómetro

Table of Contents

	Page
Introduction	88
Theoretical foundations	88
Stefan-Boltzmann law	89
Methodology	89
Instrument design	89
Characterization of the bulb	90
Results	92
Characterization of the bulb	92
Measurements with the instrument at different distances	92
Conclusions	95
Funding	96
References	96

INTRODUCTION

Currently, meteorology, particularly agricultural meteorology, utilizes very well-developed equipment. This includes the pyrgeometer, an instrument for measuring long-wave infrared radiation, whose acquisition costs are excessive, which limits energy quantification and research on radiation-atmosphere interaction, since, in order to analyze this phenomenon, it is necessary to perform precise and quantified measurements (Stoffel *et al.*, 2006).

Infrared radiation (IR), is one of the several types of radiation that conform the electromagnetic spectrum, in addition to visible and ultraviolet radiation, gamma rays, etc. The infrared band covers all wavelengths between 740 nm and 1 mm. It is possible to subdivide the IR strip into three regions based on its wavelength, as shown in Table 1.

Table 1. Spectral domain of infrared radiation

Type IR	Radiation	Wavelength – λ (μm)
Short wave	IR-A	0,76 – 2
Medium wave	IR-B	2 – 4
Long wave	IR-C	4 – 1000

Source: Valea-Pérez & Alonso-Girón, 1998.

Therefore, an instrument capable of measuring long wave radiation with components that are easily accessible in the local market was designed and built in this study, as a contribution for creating agricultural alert networks and performing energy balances and climate control in greenhouses (Gloyne & Lomas, 1980, Fairall *et al.*, 1998), thus generating greater yields in harvests and allowing to establish meteorological stations or complement existing ones.

THEORETICAL FOUNDATIONS

A black body is one that has the ability to absorb all of the radiation it receives. it also emits radiation at any temperature greater than 0 K at various wavelengths. This is possible because none of the absorbed radiation is reflected or transmitted. Hence the name, because it is due to this phenomenon that the human eye perceives these bodies to be of a deep black color (Manrique-Valadez, 2002).

Because the sun behaves as a black body with a 6.000 K surface temperature and is the main source of energy on Earth, it has become necessary to develop instruments capable of quantifying this energy in the different bands of the electromagnetic spectrum. A pyrgeometer is one of such instruments, basically composed of an appropriate housing for outdoor exposure, a transducer element

responsible for the detection of thermal infrared radiation (both from the sun and the atmosphere), and a dome that is in charge of filtering components of the electromagnetic spectrum which are outside the long-wave IR.

Stefan-Boltzmann law

The Stefan-Boltzmann law establishes a relationship between the power per unit area radiated by a black body and its surface temperature. This relationship is expressed by Equation (1).

$$E = \sigma T^4 \quad (1)$$

where σ is the Stefan-Boltzmann constant and has a value of $5,67 \times 10^{-8} \frac{W}{m^2 \cdot K^4}$ (International Unit System). This shows a large increase in the power per unit area radiated by a body in relation to its temperature (Valea-Pérez & Alonso-Girón, 1998). Equation (2) is used for a real surface (not a black body),

$$E = \varepsilon \sigma T^4 \quad (2)$$

where the emissivity coefficient is represented by ε , referring to the ability to emit radiation within a range between 0 and 1, which depends on the wavelength at which said body emits, as well as on the surface temperature (Valea-Pérez & Alonso-Girón, 1998). Due to the properties of space, there is a relationship between the power radiated by a source and the distance of the object that receives it. This relationship is established through Equation (3) (Marín-Naranjo, 2011):

$$I = \frac{P}{4\pi r^2} \quad (3)$$

where I is the irradiance of the source, P is the total radiation power emitted by the source, and r is the separation distance between the source and the receiver.

METHODOLOGY

Instrument design

The housing was made of 304 stainless steel, a material selected due to its low thermal conductivity coefficient compared to other metals, which minimizes errors caused by internal heating in the measurements of the instrument (Carbone Stainless Steel, n.d.). The housing is composed of two parts: the first one is a base with a porthole level and its corresponding screws, with the purpose of adjusting the degrees of inclination of the sensor; and the second one is the body, a hollow structure in which the circuit is located, as well as a 4-pin mini-din port for feeding and extracting information from the instrument, a Fresnel lens (a component responsible for filtering the radiation that reaches

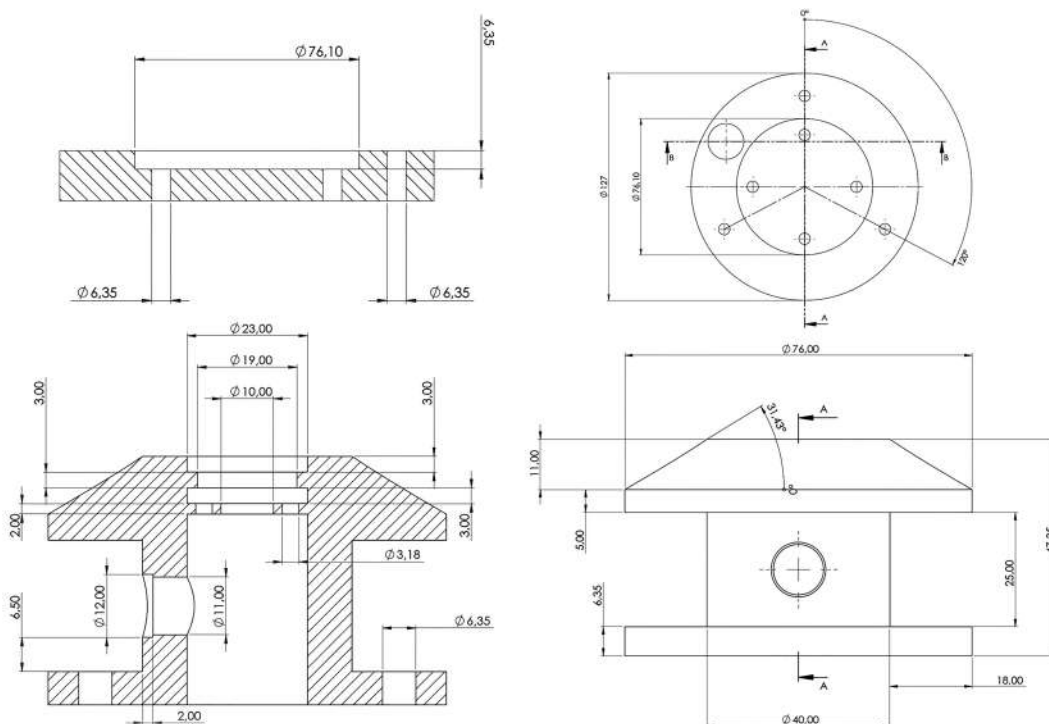


Figure 1. Plans: above, base of the instrument; down, body of the instrument

Source: Authors.

the transducer) and, inside it, silica gel, whose objective is to eliminate excess humidity. Figure 1 shows the technical specifications of the constructed housing.

The printed circuit consists of the transducer, a contactless temperature sensor manufactured by the MELEXIS company (MLX90614B), which detects the temperature by means of a thermopile. It is equipped with an optical filter which rejects radiation outside a range between 5,5 and 14 μm . The sensor output is based on an I^2C communication protocol and has a resolution of 0,02 $^{\circ}\text{C}$. (Melexis, n.d.). A necessary buffer was implemented to allow transmitting the characteristic signals of the I^2C through a shielded cable. Passive components such as a 10 $\text{K}\Omega$ resistor pair and a 0,1 μF capacitor were also included. Figure 2 is a representation of the circuit connections.

Characterization of the bulb

The first task involved determining a known radiation source. A 250 W incandescent bulb was used, which had to be characterized in order to quantify the amount of energy radiated by its tungsten filament. This bulb was disassembled to measure its dimensions, with the purpose of calculating its resistivity by means of the formula $\rho = \frac{A}{l}R$, where the resistance R is obtained from the voltage and current values measured on the bulb. Based on the data published in the article by Desai et al., 1984, the function $\rho = aT^2 + bT + c$ was obtained using a least squares approximation, where the resistivity depends on the temperature. This yields the solution of quadratic Equation (4), where the

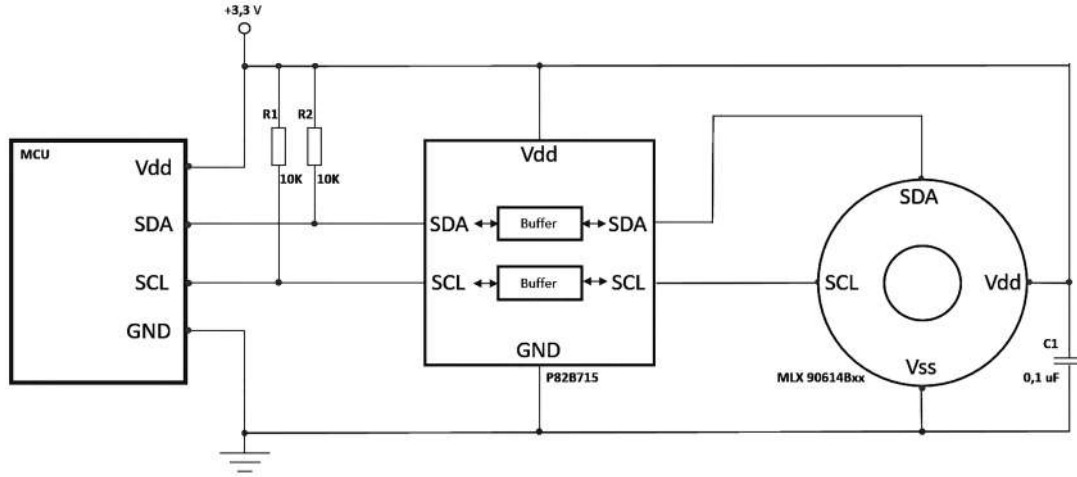


Figure 2. Connection scheme of the electronic circuit

Source: Authors.

temperature is a function of resistivity.

$$T = \frac{(-b) \pm \sqrt{b^2 - 4a(c - \rho)}}{2a} \quad (4)$$

with:

$$a = 2,783984052381960 \times 10^{-14}$$

$$\Delta a = 8,14033086876842 \times 10^{-16}$$

$$b = 2,33180658830572 \times 10^{-10}$$

$$\Delta b = 2,65298419518553 \times 10^{-12}$$

$$c = -1,08789445864861 \times 10^{-8}$$

$$\Delta c = 1,39717705908403 \times 10^{-9}$$

After obtaining the emitted temperature, the emissivity of the bulb was determined via Equation (5) (Hu & Lucyszyn, 2015), which is essential to finding its irradiance with Equation (2) and comparing it with the irradiance captured by the constructed instrument.

$$\varepsilon = (1,343 \times 10^{-4} \times T) - 2,019 \times 10^{-2} \quad (5)$$

To calibrate the instrument, a method involving the characterization of a known radiation source was used. In order to observe the behavior of the instrument according to the inverse-square law, the instrument was installed in an optimal position to capture the radiation generated by the known source. In addition, a mechanism was built with two wooden supports in order to vary the distance between the radiation source and the sensor, always with stable potential and current differences in the bulb. The experiments were performed inside a room with a heating system that allowed taking measurements within a range of atmospheric temperatures.

RESULTS

Characterization of the bulb

Table 2 shows the data obtained according to the voltage variation in the bulb regarding its characterization, which includes the calculations of resistivity, temperature, and emissivity for the radiation source.

Table 2. Data for the characterization of the bulb

V [V]	I[A]	R[Ω]	ΔR[Ω]	ρ[Ωm]	Δρ[Ω m]	T[K]	ΔT[K]	ε	I [W/m ²]
16,88	0,95	177,684	9,357E-02	2,509E-07	2,076E-08	1,003E+03	88,683	1,144E-01	6,558E+03
24,35	1,08	225,463	1,044E-01	3,184E-07	2,613E-08	1,231E+03	106,157	1,451E-01	1,890E+04
31,55	1,19	265,126	1,114E-01	3,744E-07	3,057E-08	1,414E+03	119,736	1,697E-01	3,841E+04
40,00	1,32	303,030	1,148E-01	4,279E-07	3,476E-08	1,583E+03	131,959	1,924E-01	6,843E+04
47,60	1,43	332,867	1,164E-01	4,700E-07	3,805E-08	1,712E+03	141,167	2,098E-01	1,023E+05
54,70	1,53	357,516	1,169E-01	5,048E-07	4,075E-08	1,817E+03	148,515	2,239E-01	1,385E+05
62,22	1,63	381,718	1,171E-01	5,390E-07	4,340E-08	1,919E+03	155,542	2,375E-01	1,825E+05
69,30	1,72	402,907	1,172E-01	5,689E-07	4,572E-08	2,006E+03	161,5512	2,492E-01	2,288E+05
75,60	1,79	422,346	1,180E-01	5,964E-07	4,786E-08	2,085E+03	166,991	2,598E-01	2,785E+05
85,30	1,91	446,597	1,169E-01	6,306E-07	5,050E-08	2,182E+03	173,556	2,729E-01	3,510E+05
93,70	2,00	468,500	1,172E-01	6,615E-07	5,289E-08	2,269E+03	179,412	2,845E-01	4,276E+05
100,70	2,07	486,473	1,175E-01	6,869E-07	5,487E-08	2,339E+03	184,143	2,940E-01	4,991E+05
105,00	2,12	495,283	1,168E-01	6,994E-07	5,582E-08	2,373E+03	186,402	2,986E-01	5,371E+05
108,80	2,12	513,208	1,211E-01	7,247E-07	5,784E-08	2,442E+03	191,163	3,078E-01	6,209E+05
112,50	2,15	523,256	1,217E-01	7,389E-07	5,895E-08	2,481E+03	193,736	3,130E-01	6,719E+05

Source: Authors.

Measurements with the instrument at different distances

The data taken by the sensor were recorded during the test performed with the known radiation source at a constant power of $2,5794 \times 10^2$ W, which was determined from the formula $P = A_s \varepsilon \sigma T^4$, varying the separation distances between the source and sensor. In the formula, P is the power radiated by the source, A_s is the superficial area of the tungsten filament, ε is the emissivity of the filament, σ is the Stefan-Boltzmann constant, and T is the temperature of the filament.

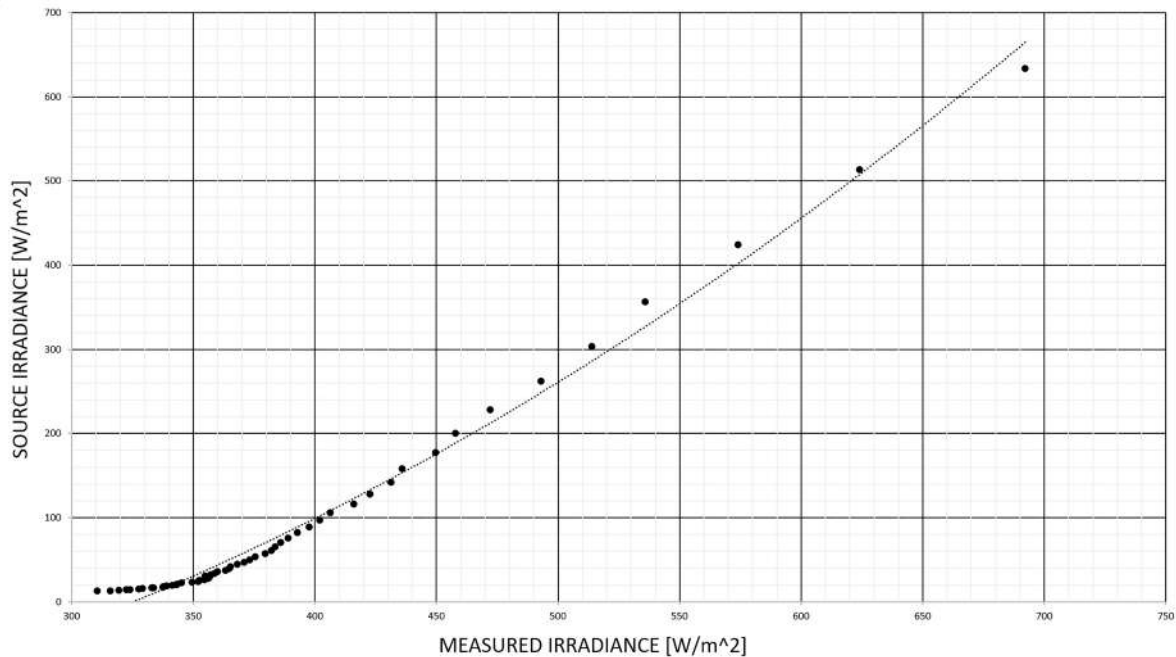


Figure 3. Expected vs. measured values (-0,97 - 59,39 °C)

Source: Authors.

In Figure 3, it is possible to identify the behavior of the sensor with respect to the radiation values emitted by the source at different distances. From the graph, a non-linear behavior is evidenced, resulting in the trend curve described by Equation (6), with a correlation coefficient $R^2 = 0,990691767716456$. This equation was used to adjust the data according to their corresponding error percentage.

$$y = 0,001663124222932x^2 + 0,120752206474762x - 215,321781365393 \quad (6)$$

A second approximation was made which consisted of separating the behavior into two regions, with the purpose of minimizing uncertainty.

Figure 4 shows the trend curve described by Equation (7), with a correlation coefficient $R^2 = 0,990066461453337$.

$$y = 0,012480906478559 x^2 - 7,97421394258089 x + 1,287,33404035389 \quad (7)$$

In the second region, the best approximation is linear (Figure 5)

The trend curve described by Equation (8) has a correlation coefficient $R^2 = 0,999046006003953$.

$$y = 1,86808371171146 x - 654,699534232818 \quad (8)$$

In Equations (7) and (8), the data were adjusted with their corresponding error percentage. Figure 6 shows the linear relationship between the measured irradiance and the inverse of the squared distance with respect to the emitting source. This, in a range of -0,97 - 59,39 °C.

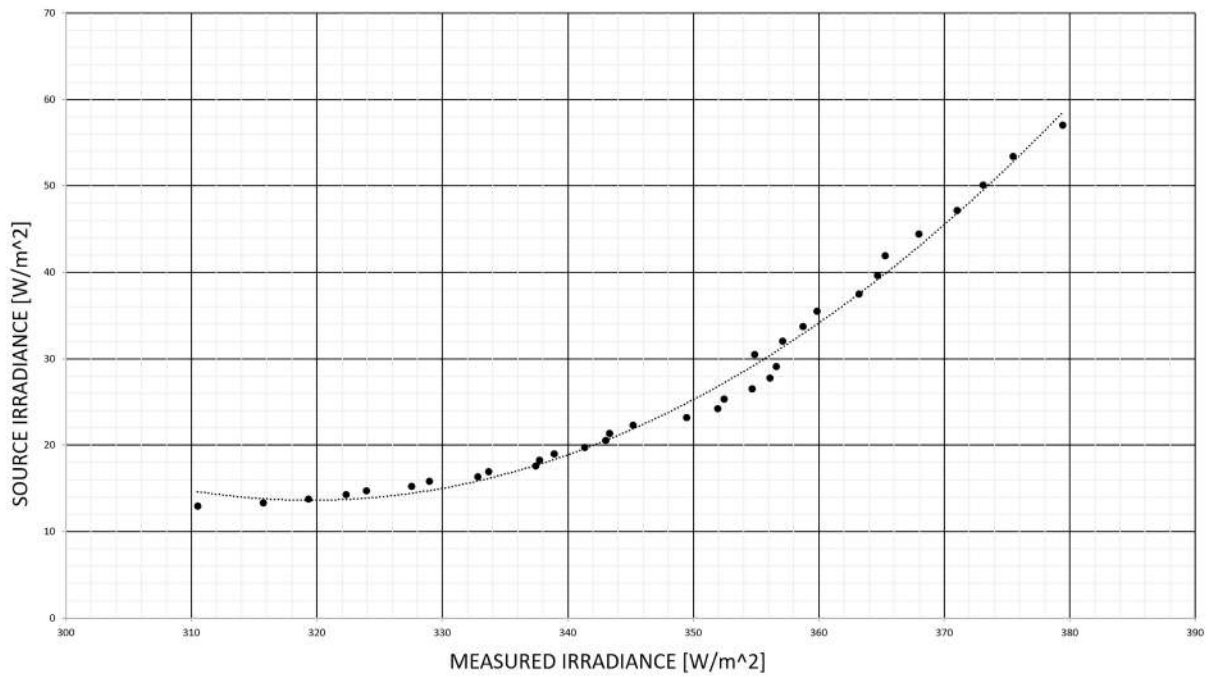


Figure 4. Expected vs. measured values (-0,97 - 13,01 °C)

Source: Authors.

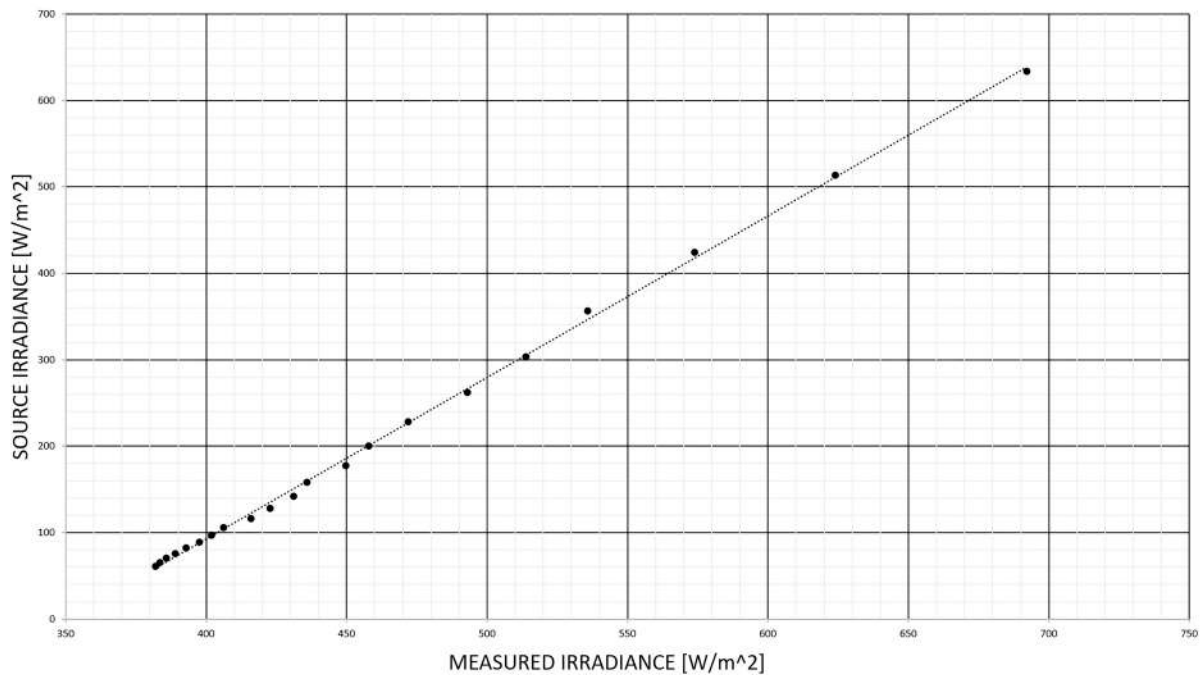


Figure 5. Expected vs. measured values (13,49 - 59,39 °C)

Source: Authors.

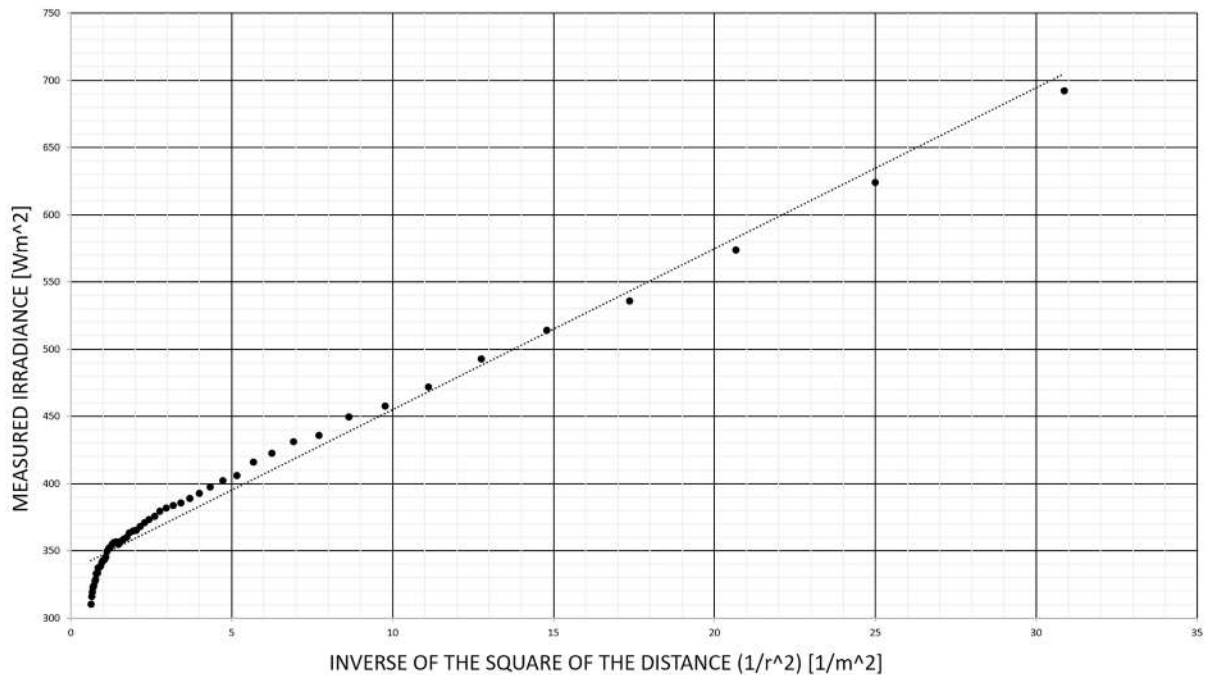


Figure 6. Radiometer behavior with regard to its distance to the source

Source: Authors.

CONCLUSIONS

The elaborated instrument shows an excellent performance in the measurement of atmospheric radiation because it has a good response in a range of atmospheric temperatures (-0,97 - 59,39 °C) at a considerably low cost (US\$ 3.000) compared to similar instruments found in the international market.

The FRESNEL lens fulfills a fundamental task in the capture and filtration of infrared radiation, thus allowing the transducer to measure correctly by concentrating the infrared thermal radiation towards it.

The characterization of the bulb served as a method to evaluate a known radiation source, through which the sensor could be reliably calibrated.

The instrument was developed with elements that are easily accessible in the national market, thus significantly reducing its production costs. The instrument can be used in the area of solar radiometry, in agricultural productivity measurements, and in instrumentation studies in the field of meteorology.

In the future, it is necessary to compare this instrument with standard equipment, given that the standard pyrgeometer of the Colombian Institute for Hydrology, Meteorology, and Environmental Studies (IDEAM) was not available for measurements.

FUNDING

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