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### SYNTHESIS OF A TRACKING CONTROL SYSTEM OVER THE FLOTATION PROCESS BASED ON LQR-ALGORITHM

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Abstract. The studies are devoted to the synthesis of the tracking control system of the flotation process based on the LQR-algorithm. The algorithm of finding the parameters of the optimal regulator is given. The results of modelling of the system with the regulator are obtained, and also the comparative analysis of the results of modelling of the system with and without the regulator is shown, which is performed with the help of Matlab software package and the Simulink toolkit.

Keywords: flotation process, optimal regulator, synthesis of the tracking system, LQR-algorithm, Matlab

### SYNTEZA NADĄŻNEGO SYSTEMU STEROWANIA PROCESEM FLOTACJI W OPARCIU O ALGORYTM LQR

Streszczenie. Badania poświęcone są syntezie nadążnego systemu sterowania procesem flotacji w oparciu o algorytm LQR. Podano algorytm wyszukiwania parametrów regulatora optymalnego. Uzyskano wyniki modelowania układu z regulatorem, a także przedstawiono analizę porównawczą wyników modelowania układu z regulatorem i bez regulatora, zrealizowaną za pomocą pakietu oprogramowania Matlab i biblioteki Simulink.

Słowa kluczowe: proces flotacji, regulator optymalny, synteza systemu nadążnego, algorytm LQR, Matlab

#### Introduction

For a long period of time, the flotation process retains a dominant role in the processing of minerals, while the scale of operations still has the tendency for an increase [5]. Foam flotation is one of the most commonly used methods for the separation of ore in the processing industry. Despite numerous researches and developments in this area, as well as potential large economic benefits that can be obtained by optimization of the enrichment process, there are still questions how to select key operational variables at which the flotation process would be more effective [3]. A flotation unit control system usually consists of ordinary single-loop controllers. However, the use and maintenance of control systems based on modern control theory has been proven as problematic in an industrial environment [7]. As a result, there were implemented expert control strategies for the logical management of situations [6]. Stable operation of flotation cells depends on the implementation of basic distributed control systems [2].

The lack of accurate measurements, nonlinear dynamics and high interaction between variables are among the main problems associated with stabilization of control. These characteristics reduce the effectiveness of control over conventional PIDregulator with manual setting in order to coordinate control loops. The use of basic distributed control often led to significant variability in the concentrate grade and its restoration, which can be observed in many concentrates around the world [1].

### 1. Problem statement

The main technological parameters in the flotation machine include: the level of pulp from the overflow threshold, the degree of aeration, the density of the pulp, the total height of the foam layer and the foam layer above the overflow threshold. In order to optimize the process of flotation of mineral raw materials, it is necessary to measure continuously and promptly the following process parameters: reagent consumption by dosing points, input and output reagent flow consumption, the pulp level in the cells of flotation machines, the degree of pulp aeration, the height of the foam layer, the specific weight of the foam layer [8]. Therefore, properly tuned and well-functioning regulators are the basis for successful control over the flotation process. The MatLab system with the Simulink extension was used as a working modelling tool. Problem statement of the optimal regulator synthesis There is presented a classical model of the control object in

the state space:

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = C^T x(t) \end{cases},$$
(1)

The control law implemented by the P-regulator is described by the formula:

$$u(t) = -k^T x(t) \tag{2}$$

One of the methods for the synthesis of regulator parameters is based on finding the minimum of the integral quadratic quality criterion:

$$I(t) = \int_0^\infty (x^T(t)Qx(t)dt + u^T(t)Ru(t))dt \to min, \quad (3)$$

For the model of the control object in the state space (1), it is necessary to synthesize the P-regulator (2), which minimizes the integral quadratic quality criterion (3).

# 2. Algorithm for finding of the optimal controller parameters

In order to solve this problem, let consider the mathematical model of the Frobenius method:

$$\begin{vmatrix} \dot{x}_1 \\ \dot{x}_2 \end{vmatrix} = \begin{vmatrix} 0 & 1 \\ -0.00002292 & -0.01241821 \end{vmatrix} \times \begin{vmatrix} x_1 \\ x_2 \end{vmatrix} + \begin{vmatrix} 0 \\ 0.00015129 \end{vmatrix} \times u(t), \tag{4}$$

Where the quality criterion has the following form:

$$I(t) = \int_0^\infty \left( \begin{vmatrix} x_1 \\ x_2 \end{vmatrix}^T \times \begin{vmatrix} 1 & 0 \\ 0 & 1 \end{vmatrix} \times \begin{vmatrix} x_1 \\ x_2 \end{vmatrix} + u^T(t) \mathbf{1}u(t) \right), \tag{5}$$

In order to implement the optimal regulator, there is used the program listing in MatLab:

>> A=[01;-0.00002292-0.01241821];

>> B=[0;0.00015129];

>> C=[1 0];

>> D=0;

>> Q=eye(2);

>> R=1;

>> sys=ss(A,B,C,D);

>> [K,S,e]=lqr(sys,Q,R)

$$\begin{split} K &= \\ 0.8599 & 52.4772 \\ S &= \\ 1.0e+05 &* \\ 0.0012 & 0.0568 \\ 0.0568 & 3.4687 \end{split}$$

-0.0102 + 0.0070i

-0.0102 - 0.0070i

where K – optimal gain matrix;

S – solution of the related Ricatti equation;

e-(A-Bk^T).

Therefore, the optimal values of the P-regulator parameters during the object control are determined by formulas (4) and (5) and will have the following form:

$$u(t) = -k^{T}x(t) = -|k_{1} \quad k_{2}| \times |x_{1}^{*1}| = -0.8599x_{1}(t) - 52.4772x_{2}(t),$$
(6)

# 3. Obtaining the modelling results of a system with a regulator

The regulator is described by a model in the state space:

$$u(t) = -k^{T}x(t) = -|k_{1} \quad k_{2}| \times \left| \begin{matrix} x_{1} \\ x_{2} \end{matrix}\right|$$

$$= -0.8599x_{1}(t) - 52.4772x_{2}(t) \quad (7)$$

$$\begin{cases} \dot{x}_{source}(t) = \begin{vmatrix} 0 & 1 \\ -0.00002292 & -0.01241821 \end{vmatrix} x(t)$$

$$\dot{x}_{closed}(t) = \begin{pmatrix} 0 & 1 \\ -0.00002292 & -0.01241821 \end{vmatrix} - \\ 0 & 1 \\ -0.00015129 \end{vmatrix} \times \\ \times |0.8599 \quad 52.4772| \\ \left\{ \dot{x}_{closed} = \begin{vmatrix} \dot{x}_{1} \\ \dot{x}_{2} \end{vmatrix} =$$

$$(8)$$

$$x(t)$$

$$x(t)$$

$$x(t)$$

 $-0.00002292x_1 - 0.01241821x_2 - 0.8599x_1 - 52.4772x_2$ , <sup>(9)</sup> The simulation scheme using the Simulink Design library is

shown on the Figure 1. In order to start the system with a regulator in the Simulink software application, you need to: connect the unit to a signal whose value you need to adjust – the permissible limits of the transition process and the steady-state value of the parameters of the controlled signal.

As a result of the simulation, the following values of the regulator parameters were proposed: k1 = -0.00002292; k2 = -0.01241821; k3 = -0.8599; k4 = -52.4772;

A simulation diagram of the comparative analysis without and with a regulator is shown on Figure 3.

Figure 1 shows a diagram of a system with a regulator, the oscilloscope displays a transition process, where the initial conditions of which negatively tend to infinity and does not coincide with the model in the state space. The Figure 4 shows a diagram of a system without a regulator, where the transition process coincides with the model in the state space and is equivalent to it.

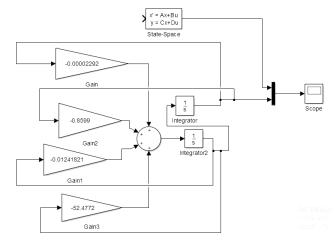
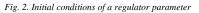


Fig. 1. Model of a system with a regulator in Simulink

🖀 Function Block Parameters: State-Space	×	🖀 Function Block Parameters: Integrator 🛛 🗙		🖀 Function Block Parameters: Integrator2			
State Space	^	Integrator		Integrator			
State-space model:		Continuous-time integration of the input signal.		Continuous-time integration of the input signal.			
dx/dt = Ax + Bu y = Cx + Du		Parameters		Parameters			
Parameters	_	External reset: none 👻		External reset: none			
A:	_	Initial condition source: internal		Initial condition source: internal 🔹			
[0 1; -0.00002292 -0.01241821]		Initial condition:		Initial condition:			
B:	_	0.5		0.2			
[0;0.00015129]		Limit output		Limit output			
C:		Wrap state		Wrap state			
[1 0]		Show saturation port		Show saturation port			
D:		Show state port		Show state port			
0		Absolute tolerance:		Absolute tolerance:			
Initial conditions:		auto		auto			
[0.5;0.2]		□ Ignore limit and reset when linearizing		Ignore limit and reset when linearizing			
Absolute tolerance:		Enable zero-crossing detection		Enable zero-crossing detection			
auto		State Name: (e.g., 'position')		State Name: (e.g., 'position')			
State Name: (e.g., 'position')		П		n l			
п	<b>~</b>		~	· · · · · · · · · · · · · · · · · · ·			
QK <u>C</u> ancel <u>H</u> elp Ap	ply	QK Cancel Help Apply		OK Cancel Help Apply			



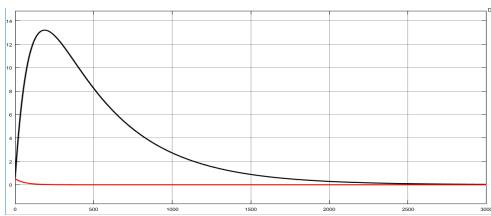


Fig. 3. System parameter process with and without a regulator

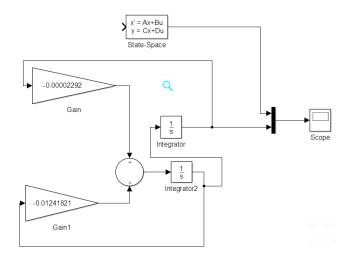


Fig. 4. Diagram of a system without a regulator in Simulink

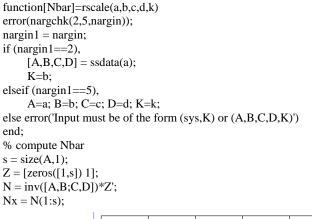
### 4. Synthesis of the servo system

**60** 

The method of analytical construction of regulators according to the criterion of generalized operation (AKOR), developed by A.A. Krasovsky, allows the synthesis of regulators for objects described by systems of ordinary nonlinear differential equations of higher order, which compares favourably with many other methods for the synthesis of optimal regulators [4]. In this case, the mathematical model of the control object in the most general case has the form:

$$\begin{cases} \dot{x}(t) = Ax(t) + B(-k^T x(t)) + B * Nbar * r(t) \\ y(t) = C^T x(t) \end{cases}, \quad (10)$$

In order to obtain the simulation result of the servo system, it is necessary to create a file-function:



Nu = N(1+s);Nbar=Nu + K\*Nx;

Let save the program as rscale.m. After this process, we get the number Nbar in MatLab:

>> Nbar=rscale(sys,K)

Nbar =

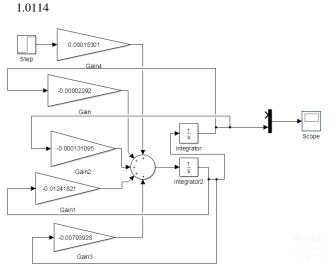
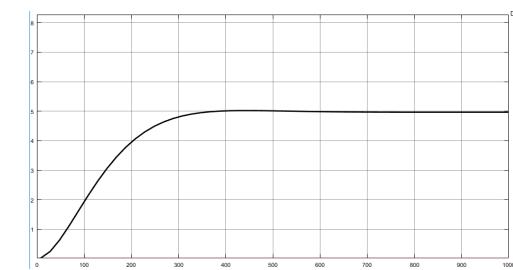


Fig. 5. Servo system model in Simulink

Step					
Output a step.					
Parameters					
Step time:					
0					
Initial value:					
0					
Final value:					
5					
Sample time:					
0					
✓ Interpret vector paramet	ters as 1	-D			
Enable zero-crossing det	tection				
	<u>)</u> K	Cancel	<u>H</u> elp	_	<u>A</u> pply





Therefore, the optimal parameters of the regulator are solved. There are presented the system simulation algorithms with and without a regulator. Was developed a synthesis of a servo control system over the flotation process based on the LQR - algorithm. Solving the problem of choosing the optimal regulator parameters, it is necessary to check whether the system under study is controlled and observable. If not, then the synthesis is impossible. Obviously, in order to determine these properties, the A, B, C – equations matrices of variable states are used that characterize the input and output parameters of the mode of the system under study.

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