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TWO-PHASE WITH NON-STANDARD EFFECTS STABILITY EQUATIONS OF FLOWS

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Introduction

The paper takes into account the unstable effects of the interaction forces of the phases in deriving the stability equations of two-phase currents. In a straight-line nonstationary motion of a disperse mixture, the forces acting on the particle can be given in the form

$$(1 - \alpha)\rho_1 \left(\frac{\partial \hat{v}}{\partial \hat{t}} + \hat{v} \hat{v} \hat{v} \right) = -(1 - \alpha) \hat{v} \hat{p} + \alpha \frac{9}{2} \frac{\mu}{a^2} (\hat{u} - \hat{v}) + \\ + \mu \hat{v} \hat{v} \hat{u} - \frac{4}{3} \pi a^3 \rho_1 \frac{\partial \hat{v}}{\partial \hat{t}} + \frac{2}{3} \pi a^3 \rho_1 \frac{\partial}{\partial \hat{t}} (\hat{u} - \hat{v}) + \\ + 6a^2 \sqrt{\pi \rho_1 \mu} \int_{-\infty}^{\hat{t}} \frac{\partial}{\partial \tau} (\hat{u} - \hat{v}) \frac{\partial \tau}{\sqrt{\hat{t} - \tau}}, \quad (1)$$

$$\frac{\partial(1-\alpha)}{\partial \hat{t}} + \hat{v}(1-\alpha)\hat{v} = 0, \quad (2)$$

$$\alpha \rho_2 \left(\frac{\partial \hat{u}}{\partial \hat{t}} + \hat{u} \cdot \hat{v} \hat{u} \right) = -\alpha \hat{v} \hat{p} + \alpha \frac{9}{2} \frac{\mu}{a^2} (\hat{v} - \hat{u}) + \frac{4}{3} \pi a^3 \rho_1 \frac{\partial \hat{v}}{\partial \hat{t}} + \frac{2}{3} \pi a^3 \rho_1 \frac{\partial}{\partial \hat{t}} (\hat{v} - \hat{u}) + \\ + 6a^2 \sqrt{\pi \rho_1 \mu} \int_{-\infty}^{\hat{t}} \frac{\partial}{\partial \tau} (\hat{v} - \hat{u}) \frac{d\tau}{\sqrt{\hat{t} - \tau}}, \quad (3)$$

$$\frac{\partial \alpha}{\partial \hat{t}} + \hat{v} \cdot \alpha \hat{u} = 0. \quad (4)$$

To write these equations in dimensionless form, we introduce the following definitions:

$$\hat{v} = Vv, \hat{u} = Uu, \hat{t} = \frac{t}{\omega}, \hat{x} = Lx, \hat{y} = Ly.$$

(1)–(4) – we accept these assumptions to solve the equations [1,2,3,4,5,6,7]:

1) particles are spherical and their motion obeys Stokes' law;

of the sum of the adhesive friction force, the Archimedean force, the added mass force Basse forces. For a heterogeneous environment [1] the conservation equations proposed in the literature are as follows:

2) since the volumetric concentration of particles $a \ll 1$ is considered small, the interaction between individual particles is not taken into account;

3) The einstein correction of the viscosity, which is proportional to the volumetric concentration of the particle, is ignored.

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When such assumptions are taken into account, written in dimensionless form, equations (1) - (4) have the following form [1].

$$(1 - \alpha) \left(\frac{\partial v}{\partial t} + (v \cdot \nabla) v \right) = -(1 - \alpha) \nabla p + \alpha \frac{S_1}{\tau} (u - v) + \frac{1}{2} \alpha \frac{\partial}{\partial t} (u - v) - \alpha \frac{\partial v}{\partial t} + \sqrt{\frac{g}{2\pi}} \alpha \sqrt{\frac{S_1}{\tau}} \int_{-\infty}^t \frac{\partial}{\partial \tau} (u - v) \frac{d\tau}{\sqrt{\tau-t}} + \frac{1}{Re} \nabla^2 v, \quad (5)$$

$$\frac{\partial(1-\alpha)}{\partial t} + \nabla \cdot (1 - \alpha)v = 0, \quad (6)$$

$$\alpha \left(\frac{\partial u}{\partial t} + (u \cdot \nabla) u \right) = -\frac{\alpha}{S_1} \nabla p + \frac{\alpha}{\tau} (v - u) + \frac{1}{2} \frac{\alpha}{S_1} \frac{\partial}{\partial t} (v - u) + \frac{\alpha}{S_1} \frac{\partial v}{\partial t} + \sqrt{\frac{g}{2\pi \tau S_1}} \int_{-\infty}^t \frac{\partial}{\partial \tau} (v - u) \frac{d\tau}{\sqrt{\tau-t}}, \quad (7)$$

$$\frac{\partial \alpha}{\partial t} + \nabla \cdot \alpha u = 0, \quad (8)$$

here $v = (v_1, v_2)$, $u = (u_1, u_2)$ – velocity vectors for pure gas and particles, respectively; p – pressure, $S_1 = \frac{\rho_2}{\rho_1}$ density ratio, ρ_1 – density of pure gas, ρ_2 – particle material density, $\tau = SRe$ – dimensionless size - the relaxation time of the particles, $Re = \frac{\rho_1 U_0 L}{\mu}$

– Reynolds number, $S = \frac{2}{9} \left(\frac{a}{L}\right)^2 \frac{\rho_2}{\rho_1}$ size here a - particle radius, L – half the width of the channel, U_0 – characteristic velocity of flow, μ – viscosity coefficient, $\nabla = \frac{\partial}{\partial x} i + \frac{\partial}{\partial y} j$, $\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$ – Laplace operators.

$$(1 - \alpha_0) \left(\frac{\partial V'}{\partial t} + V \frac{\partial V'}{\partial t} + V'_2 \frac{\partial V}{\partial t} i \right) = -(1 - \alpha_0) \nabla p' + \alpha_0' \nabla p_0 + \alpha_0 \frac{S_1}{\tau} (u' - v') + \frac{1}{2} \alpha_0 \frac{\partial}{\partial t} (u' - v') - \alpha_0 \frac{\partial V'}{\partial t} + \alpha_0 \sqrt{\frac{g}{2\pi}} \sqrt{\frac{S_1}{\tau}} \int_{-\infty}^t \frac{\partial}{\partial \tau} (u' - v') \frac{d\tau}{\sqrt{\tau-t}} + \frac{1}{Re} \nabla^2 V' \quad (9)$$

$$-\frac{\partial \alpha_0'}{\partial t} + (1 - \alpha_0) \nabla \cdot V' + V \frac{\partial \alpha_0'}{\partial x} = 0, \quad (10)$$

$$\frac{\partial u'}{\partial t} + V \frac{\partial u'}{\partial x} + u'_2 \frac{\partial v}{\partial y} i = \frac{1}{S_1} \nabla p' + \frac{1}{\tau} (V' - u') + \frac{1}{2S_1} \frac{\partial}{\partial t} (V' - u') + \frac{1}{S_1} \frac{\partial v'}{\partial t} + \sqrt{\frac{g}{2\pi \tau S_1}} \int_{-\infty}^t \frac{\partial}{\partial \tau} (V' - u') \frac{d\tau}{\sqrt{\tau-t}}, \quad (11)$$

$$\frac{\partial \alpha_0'}{\partial t} + \alpha_0 \nabla \cdot u' + \nabla \frac{\partial \alpha_0'}{\partial x} = 0. \quad (12)$$

(9)-(12) – we look for the solutions of the equations in the following form:

$$\begin{bmatrix} v' \\ u' \\ p' \\ \alpha' \end{bmatrix} = \begin{bmatrix} v'_0(y) \\ u'_0(y) \\ p'_0(y) \\ \alpha'_0(y) \end{bmatrix} e^{i(kx - \omega t)} \quad (13)$$

(13) – equation (9) - (12) after we lose the pressure, we get:

$$\begin{aligned} & -i\omega \left(ikV'_{20} - \frac{\partial V'_{10}}{\partial y} \right) + ikV \left(ikV'_{20} - \frac{\partial V'_{20}}{\partial y} \right) - ikV'_{10} \frac{\partial V}{\partial y} - V'_{20} \frac{\partial^2 V}{\partial y^2} - \frac{\partial V'_{20}}{\partial y} \frac{\partial V}{\partial y} = \\ & = \frac{\alpha_0}{1-\alpha_0} \frac{g}{\tau} \left[\left(iku'_{20} - \frac{\partial u'_{10}}{\partial y} \right) - \left(ikV'_{20} - \frac{\partial V'_{10}}{\partial y} \right) \right] - \frac{1}{2} \frac{\alpha_0}{1-\alpha_0} i\omega \left[\left(iku'_{20} - \frac{\partial u'_{10}}{\partial y} \right) - \left(ikV'_{20} - \frac{\partial V'_{10}}{\partial y} \right) \right] + \\ & + \frac{\alpha_0}{1-\alpha_0} i\omega \left(ikV'_{20} - \frac{\partial V'_{10}}{\partial y} \right) + \frac{3\alpha_0}{2(1-\alpha_0)} \sqrt{\frac{S_1}{\tau}} \sqrt{\omega} (1-i) \left[\left(iku'_{20} - \frac{\partial u'_{10}}{\partial y} \right) - \left(ikV'_{20} - \frac{\partial V'_{10}}{\partial y} \right) \right] + \\ & + \frac{1}{1-\alpha_0} \frac{1}{Re} \left[\left(\frac{\partial^2}{\partial y^2} - k^2 \right) (ikV'_{20} - \frac{\partial V'_{10}}{\partial y}) \right], \end{aligned} \quad (14)$$

$$i\omega \alpha'_0 + (1 - \alpha) \left(ikv'_{10} + \frac{\partial v'_{20}}{\partial y} \right) + v \cdot ik\alpha'_0 = 0, \quad (15)$$

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$$u'_{20} \frac{\partial^2 V}{\partial y^2} - \frac{\partial u'_{20}}{\partial y} \frac{\partial V}{\partial y} = \frac{1}{\tau} \left[\left(ikv'_{20} - \frac{\partial v'_{10}}{\partial y} \right) - \left(iku'_{20} - \frac{\partial u'_{10}}{\partial y} \right) \right] - \frac{1}{2S_1} i\omega \left[\left(ikv'_{20} - \frac{\partial v'_{10}}{\partial y} \right) + \frac{3}{2} \frac{1}{\sqrt{\tau S_1}} \sqrt{\omega} (1 - i) \left[\left(ikv'_{20} - \frac{\partial v'_{10}}{\partial y} \right) - \left(iku'_{20} - \frac{\partial u'_{10}}{\partial y} \right) \right] \right], \quad (16)$$

$$-i\omega\alpha'_0 + \alpha_0 \left(iku'_{10} + \frac{\partial u'_{20}}{\partial y} \right) + v \cdot ik\alpha'_0 = 0. \quad (17)$$

(17) - as can be seen from the equation, if the excitation u'_0 specific amplitude of velocity $\delta \ll 1$ If the size, then $\alpha'_0 \approx 0(\alpha_0\delta)$ the order size will be here $\alpha_0 \ll 1$. Therefore, as in the [2,3,4,5,6,7] literature, we are at the first approach (14) - (17) in systems α'_0 participating participants $\alpha'_0 = 0$ assuming that we cannot ignore it. In this case, it is convenient to

$$D^2\psi - ik \operatorname{Re} \left(V - \lambda - \frac{if}{k\tau} \right) D\psi + ik \operatorname{Re} \frac{d^2V}{dy^2} \psi + \frac{f}{S} D\varphi - i\lambda k \frac{f}{2S_1} (D\varphi - D\psi) + \\ + i\lambda k \frac{f}{S_1} D\psi - \frac{3}{2} \operatorname{Re} f \sqrt{\frac{k}{S_1\tau}} (i - 1)\sqrt{\lambda} (D\psi - D\varphi) = 0, \quad (18)$$

$$D\psi - ik\tau \left(U - \lambda - \frac{i}{k\tau} \right) D\varphi + ik\tau \frac{d^2U}{dy^2} \varphi - i\lambda \frac{k}{2S_1} (\partial\psi - \partial\varphi) - i\lambda \frac{k}{S_1} D\varphi - \\ - \frac{3}{2} \sqrt{\frac{k\tau}{S_1}} (i - 1) \sqrt{\lambda} (D\varphi - D\psi) = 0, \quad (19)$$

here $D = \frac{\partial^2}{\partial y^2} - k^2$, $\lambda = \frac{\omega}{k}$, k - number of waves, $\lambda = \lambda_r + i\lambda_i$ - unknown constant to be determined, λ_r - phase speed, λ_i - growth rate, $f = \alpha_0 S_1$ - the mass-specific concentration of particles, if $\lambda_i > 0$ the current will not be constant, otherwise $\lambda_i < 0$ is stable when $\lambda_i = 0$ if so, the vibration will be neutral constant.

(18) and (19) in the equations $V(y)$ and $U(y)$ the stationary flow rates of pure gas and particles are determined accordingly.

introduce two current functions to integrate the continuity equations (15) and (17).

$$-v'_{10} = \frac{\partial\psi}{\partial y}, \quad v'_{20} = ik\psi, \\ -u'_{10} = \frac{\partial\varphi}{\partial y}, \quad u'_{20} = ik\varphi.$$

In this case, equations (14) - (17) take the following form:

$$D^2\psi - ik \operatorname{Re} \left(V - \lambda - \frac{if}{k\tau} \right) D\psi + ik \operatorname{Re} \frac{d^2V}{dy^2} \psi + \frac{f}{S} D\varphi - i\lambda k \frac{f}{2S_1} (D\varphi - D\psi) + \\ + i\lambda k \frac{f}{S_1} D\psi - \frac{3}{2} \operatorname{Re} f \sqrt{\frac{k}{S_1\tau}} (i - 1)\sqrt{\lambda} (D\psi - D\varphi) = 0, \quad (18)$$

The boundary conditions for the movements in the Poiseuille stream are as follows:

$$\psi(\pm 1) = \frac{d\psi}{dy}(\pm 1) = 0, \quad (20)$$

$$\varphi(\pm 1) = 0. \quad (21)$$

For pure gas, equation (20) represents the normal condition of impermeability and viscosity, while for solid particles, equivalence condition (21) represents equality.

References:

- Nigmatulin, R.I. (1987). *Dynamics of multiphase media. T.I.* (p.464). Moscow: Nauka.
- Drew, D.A. (1979). Stability of a Stokes layer of a dusty gas. - *Phys. Fluids*, v.22, № 11, pp. 2081-2086.
- Narmuratov, Ch.B., & Solovyov, A.S. (1986). On the influence of suspended particles on the stability of the plane Poiseuille flow. *Izvestia of the USSR Academy of Sciences, MZhG*, No. 1, M., 46-53.
- Chuliayev, E.A., Khakimov, A., & Shoniev, F.A. (2007). On mathematical models of hydrodynamic stability of multiphase flows. *Mining Bulletin of Uzbekistan*, No. 29, pp.115-116.
- Narmuratov, Ch.B., Chuliayev, E.A., & Khuzhayorov, B.Kh. (1998). Stability of the boundary layer of two-phase flows taking into account the Stokes and Archimedes forces. *Uzbek magazine "Problems of Mechanics"*, Tashkent, No. 4.
- Narmuratov, Ch.B., Chuliayev, E.A., & Khuzhayorov, B.Kh. (1998). Influence of the Stokes and Archimedes force on the stability of a two-phase Poiseuille flow. *Reports of the Academy of Sciences of the Republic of Uzbekistan*, Tashkent, No. 2.
- Narmuratov, Ch.B., & Chuliayev, E.A. (1995). *Stability equations of two-phase currents, taking into account the unstable effects of the*

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- interaction forces of the phases. Sb. nauch. tr. SamGU. (pp.23-29). Samarkand.
8. M. O. K. (2021). To Arouse Students' Interest in National Music by Informing them about Shashmaqom Branches. *International Journal on Orange Technologies*, 3(12), 30-34. <https://doi.org/10.31149/ijot.v3i12.2447>
9. E., R. N., & H., X. B. (2021). Learning the Flora of Kuljuktov. *International Journal on Orange Technologies*, 3(12), 30-34. <https://doi.org/10.31149/ijot.v3i12.2443>
10. Qubbijonovich, Q. T. (2021). The Interdependence of Types of Musical Activities in Music Culture Classes. *International Journal on Orange Technologies*, 3(12), 10-15. <https://doi.org/10.31149/ijot.v3i12.2444>