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M.Sc.Eng., Corresponding Member of International Academy of Theoretical and Applied Sciences, Lecturer,

Denis Chemezov

Vladimir Industrial College

Russian Federation

<https://orcid.org/0000-0002-2747-552X>

vic-science@yandex.ru

Oleg Stepanov

Vladimir Industrial College

Student, Russian Federation

Lyubov Suvorova

Vladimir Industrial College

Student, Russian Federation

Aleksey Matankin

Vladimir Industrial College

Student, Russian Federation

Vadim Maksimov

Vladimir Industrial College

Student, Russian Federation

Aleksey Kuzin

Vladimir Industrial College

Student, Russian Federation

Nikita Muzychenko

Vladimir Industrial College

Student, Russian Federation

THE DEFORMATION DEGREE OF VARIOUS MATERIALS DURING THE COMPRESSION TEST

Abstract: The results of the computer calculation of the compression process of the standard specimens made of aluminum, copper, armco iron, cast iron, ceramics and concrete are presented in the article. The analysis of the compression ratio of materials under conditions of shortening the specimen height by 50% from the initial height was performed. It is determined that the greatest degree of compression is observed during deformation of the specimens made of aluminum and concrete.

Key words: the specimen, the compression test, deformation, ratio.

Language: English

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Introduction

Compression of the standard specimens is performed to determine the mechanical properties of brittle and ductile materials (for example, the compressive strength) [1]. The strength of material can be determined by the degree of volumetric deformation (fracture) of the specimen under the action of the applied load [2]. The analysis of fracture of the cast iron specimens during compression on the testing machine was performed in the work [3]. The specimen shortening under the load by 30% from the initial height leads to partial fracture of material (the symmetrical formation of cracks by the diameter at the angle of 50 degrees relative to the centerline of the specimen). Taking into account the fact that the nature of the cracks formation in the specimen on both sides is different, it can be concluded that the intensity of compression deformation of material along the section is different. The degree of compression deformation of brittle and ductile materials can be determined by

the mathematical calculation of the dynamics of the compression process of the specimens on the computer. The ratio value will reveal the percentage of volumetric deformation of material during compression.

Materials and methods

The computer calculation of the compression process of the specimens models made of aluminum, copper, concrete, cast iron, armco iron and ceramics was implemented in the ANSYS Autodyn 14.5 program [4]. The specimens models were cylinders with the diameter of 4 mm and the height of 4.5 mm. Each specimen was subjected to the variable load applied to the free from basing the end surface of the model. Deformation of the specimens models was carried out in accordance with the Lagrangian formulation. The materials properties of the specimens and the compression test scheme are presented in the table 1 and in the Fig. 1, respectively.

Table 1. The materials properties and the compression test scheme of the specimens.

Aluminum [5]			Concrete (compressive strength is 25 MPa) [6]		
	Reference density		2.71 g/cm ³	Reference density	2.75 g/cm ³
EOS	Equation	Shock	Equation	<i>P</i> alpha	
	Gruneisen coefficient	2.1	Porous density	2.314 g/cm ³	
	Parameter <i>CI</i>	5.38×10 ³ m/s	Porous sound speed	2.92×10 ³ m/s	
	Parameter <i>SI</i>	1.337	Initial compaction pressure	2.33×10 ⁴ kPa	
Strength	Equation	von Mises	Solid compaction pressure	6.0×10 ⁶ kPa	
	Shear modulus	2.69×10 ⁷ kPa	Compaction exponent	3.0	
	Yield stress	2.9×10 ⁵ kPa	Solid EOS	Polynomial	
Iron-C.E.		EOS	Bulk modulus <i>A1</i>	3.527×10 ⁷ kPa	
	Reference density		7.89 g/cm ³	Parameter <i>A2</i>	3.958×10 ⁷ kPa
EOS	Equation		Linear	Parameter <i>A3</i>	9.04×10 ⁶ kPa
	Bulk modulus		1.64×10 ⁸ kPa	Parameter <i>B0</i>	1.22
	Reference temperature		300 K	Parameter <i>B1</i>	1.22
	Specific heat		452.0 J/(kg×K)	Parameter <i>T1</i>	3.527×10 ⁷ kPa
Strength	Equation		Johnson-Cook	Reference temperature	300 K
	Shear modulus		8.0×10 ⁷ kPa	Specific heat	654.0 J/(kg×K)
	Yield stress		2.9×10 ⁵ kPa	Compaction curve	Standard
	Hardening constant		3.39×10 ⁵ kPa	Equation	<i>RHT</i> concrete
	Hardening exponent	0.4	Shear modulus	1.67×10 ⁷ kPa	
	Strain rate constant	0.055	Compressive strength (<i>f_c</i>)	3.5×10 ⁴ kPa	
	Thermal softening exponent	0.55	Tensile strength (<i>f_t/f_c</i>)	0.1	
	Melting temperature	1.811×10 ³ K	Shear strength (<i>f_s/f_c</i>)	0.18	
	Ref. strain rate (/s)	1.0	Intact failure surface constant <i>A</i>	1.6	
Strain rate correction	1 st order	Intact failure surface exponent <i>N</i>	0.61		
Al ₂ O ₃ [7-8]		Strength	Tens./comp. meridian ratio (<i>Q</i>)	0.6805	
	Reference density		3.9 g/cm ³	Brittle to ductile transition	0.0105
EOS	Equation		Shock	<i>G</i> (elas.)/(elas.-plas.)	2.0
	Gruneisen coefficient		0.5	Elastic strength/ <i>f_t</i>	0.7
	Parameter <i>CI</i>		6.9×10 ³ m/s	Elastic strength/ <i>f_c</i>	0.53

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Strength	Parameter <i>SI</i>	1.45		Fractured strength constant <i>B</i>	1.6	
	Equation	von Mises		Fractured strength exponent <i>M</i>	0.61	
	Shear modulus	1.0×10 ⁸ kPa		Compressive strain rate exp. alpha	0.032	
	Yield stress	8.0×10 ⁶ kPa		Tensile strain rate exp. delta	0.036	
Armco iron [10]						
EOS	Reference density	7.87 g/cm ³	Failure	Equation	<i>RHT</i> concrete	
	Equation	Linear		Damage constant, <i>D1</i>	0.04	
	Bulk modulus	1.64×10 ⁸ kPa		Damage constant, <i>D2</i>	1.0	
	Reference temperature	300 K		Minimum strain to failure	0.01	
	Specific heat	452.0 J/(kg×K)		Residual shear modulus fraction	0.13	
Strength	Equation	Johnson-Cook	Erosion	Tensile failure	Hydro (<i>P_{min}</i>)	
	Shear modulus	8.0×10 ⁷ kPa		Equation	Geometric strain	
	Yield stress	1.75×10 ⁵ kPa		Erosion strain	2.0	
	Hardening constant	3.8×10 ⁵ kPa	Type of geometric strain	Instantaneous	Copper [9]	
	Hardening exponent	0.32	Reference density		8.9 g/cm ³	
	Strain rate constant	0.06	EOS	Equation	Shock	
	Thermal softening exponent	0.55		Gruneisen coefficient	2.0	
	Melting temperature	1.811×10 ³ K		Parameter <i>CI</i>	3.958×10 ³ m/s	
	Ref. strain rate (/s)	1.0		Parameter <i>SI</i>	1.497	
	Strain rate correction	1 st order		Reference temperature	300 K	
Failure	Equation	Johnson-Cook	Strength	Equation	Piecewise JC	
	Damage constant, <i>D1</i>	-2.2		Shear modulus	4.64×10 ⁷ kPa	
	Damage constant, <i>D2</i>	5.43		Yield stress (zero plastic strain)	1.2×10 ⁵ kPa	
	Damage constant, <i>D3</i>	-0.47		Eff. plastic strain #1	0.3	
	Damage constant, <i>D4</i>	0.016		Eff. plastic strain #2	1.0×10 ²⁰	
	Damage constant, <i>D5</i>	0.63		Yield stress #1	4.5×10 ⁵ kPa	
	Melting temperature	1.811×10 ³ K		Yield stress #2	4.5×10 ⁵ kPa	
	Ref. strain rate (/s)	1.0		Thermal softening exponent	1.0	
		Melting temperature	1.0×10 ²⁰ K			
		Ref. strain rate (/s)	1.0			

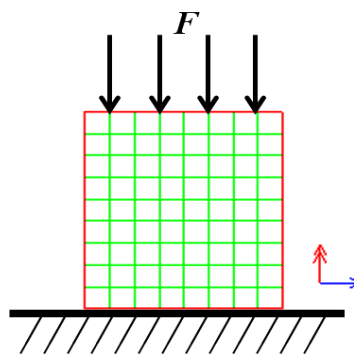


Figure 1 – The compression test scheme.

Results and discussion

Modeling the compression process was performed before shortening the model height by 50% from the initial height of the specimen. The calculated values of the compression ratio were obtained along the axis of the deformed specimen. The distance values on the graph are presented by the height values

of the deformed specimen. The zero value for this coordinate axis of the graph is the reference point of the specimen height from the side of the applied load. The dependencies of the compression ratio of materials on the height of the deformed specimens are presented in the Fig. 2.

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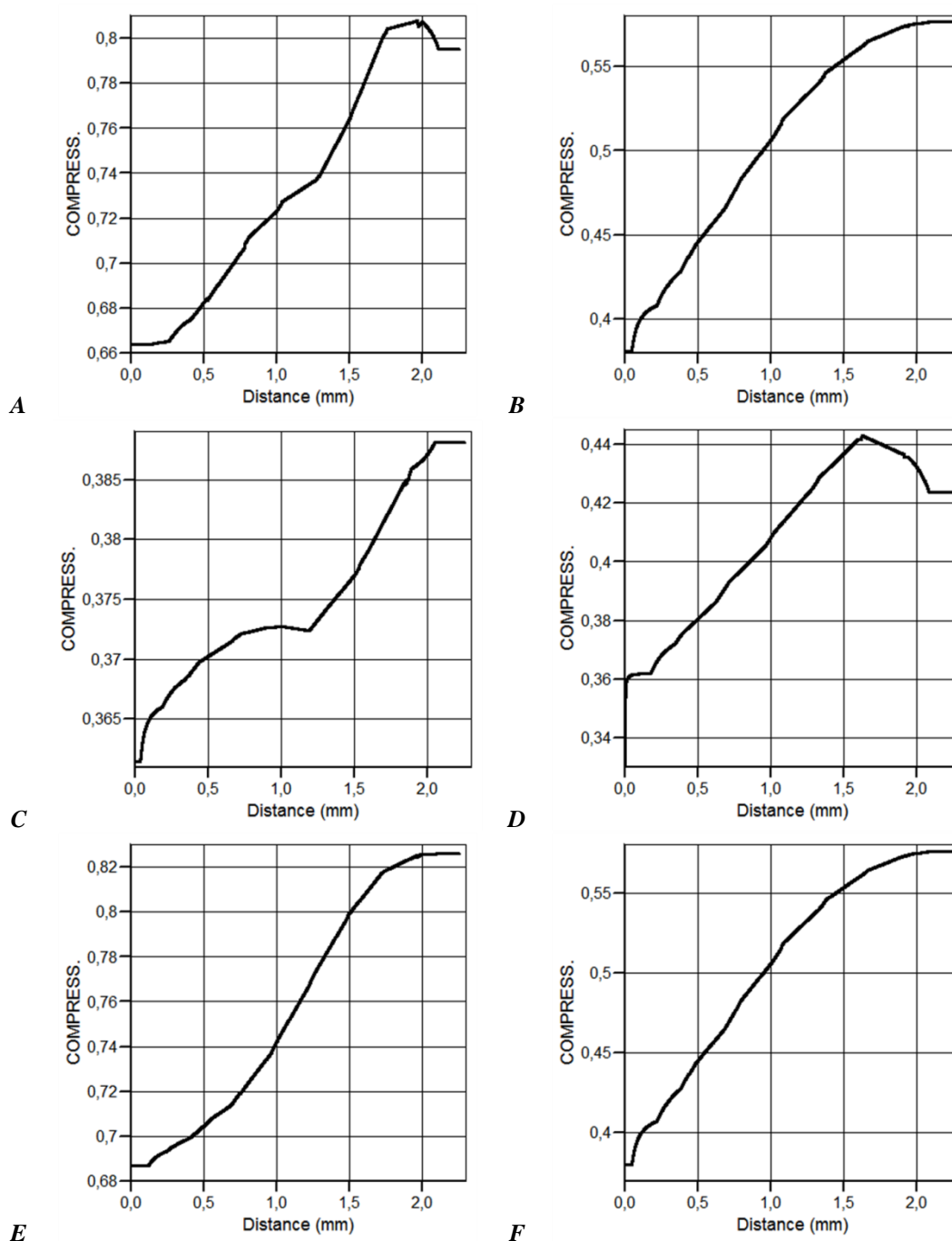


Figure 2 – The dependencies of the compression ratio of materials on the height of the deformed specimens: A – aluminum; B – iron-C.E.; C – Al₂O₃; D – copper; E – concrete (the compressive strength is 25 MPa); F – armco iron.

After analyzing the obtained graphs, it was determined that the greatest compressive strength is observed in the specimen made of ceramics. The compression ratio of ceramics during corresponding deformation is 0.39. In this case, the change range of the ratio value over the entire cross section of the specimen is no more than 0.03. This minimal change in the ratio value indicates the most uniform compression of material over the entire volume of the

specimen. The lowest compressive strength is observed in the specimens made of aluminum and concrete. The compression ratio of these materials during corresponding deformation is 0.81 and 0.83, respectively. The change range of the compression ratios of aluminum and concrete increases by 5 times compared to ceramics. Iron-containing alloys are subjected to compression deformation in the same way and have the average values of the ratios. All

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materials are characterized by an increase in the compression ratio in the direction from the end surface on which the load is applied to the end surface on which basing the specimen is performed.

Conclusion

Thus, aluminum and concrete are destroyed during compression deformation of the volume by

50%, since the calculated compression ratio is 0.81-0.83 of 1.0 (where 1.0 is total failure of material). Compression of the ceramic products does not lead to the formation of significant change in the values of internal deformations in the volume. This indicates almost the same properties over the entire volume of deformed material. The compression ratio of ceramics is 0.39, which is half that of aluminum and concrete.

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